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Basic principles of neonatal bubble CPAP: effects on CPAP delivery and imposed work of breathing when altering the original design

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ABSTRACT

Background The original bubble continuous positive airway pressure (bCPAP) design has wide-bore tubing and a low-resistance interface. This creates a stable airway pressure that is reflected by the submersion depth of the expiratory tubing. Several systems with alterations to the original bCPAP design are now available. Most of these are aimed for use in low-income and middle-income countries and have not been compared with the original design.

Objective We identified three major alterations to the original bCPAP design: (1) resistance of nasal interface, (2) volume of dead space and (3) diameter of expiratory tubing. Our aim was to study the effect of these alterations on CPAP delivery and work of breathing in a mechanical lung model. Dead space should always be avoided and was not further tested.

Methods The effect of nasal interface resistance and expiratory tubing diameter was evaluated with simulated breathing in a mechanical lung model without interface leakage. The main outcome was delivered CPAP and imposed work of breathing.

Results High-resistance interfaces and narrow expiratory tubing increased the work of breathing. Additionally, narrow expiratory tubing resulted in higher CPAP levels than indicated by the submersion depth.

Conclusion Our study shows the significant effect on CPAP delivery and imposed work of breathing when using high-resistance interfaces and narrow expiratory tubing in bCPAP systems. New systems should include low-resistance interfaces and wide-bore tubing and be compared with the original bCPAP. Referring to all systems that bubble as bCPAP is misleading and potentially hazardous.

INTRODUCTION

Every year, an estimated 15 million babies are born preterm.¹ Complications of preterm birth is the leading cause of neonatal mortality, and the WHO estimates that three out of four of these babies can be saved with improved maternal and neonatal care. The use of continuous positive airway pressure (CPAP) is one of the recommended interventions to reduce morbidity and mortality in preterm infants.^{2,3}

In 1971, Gregory *et al* introduced the first CPAP system intended for neonatal use.⁴ The distending pressure was created by a resistor clamp on the system expiratory limb. It had a water submersion pop-off pressure valve set at 30 cmH₂O and has

What is already known on this topic?

- In its original design with low-resistance interface and wide-bore expiratory tubing, the bubble continuous positive airway pressure (bCPAP) is pressure stable and easy to breathe through.
- In 2012, WHO noted that many devices were homemade or developed specifically for low-income countries and needed to be tested for durability, reliability and safety.
- Alterations to the original bCPAP design include high-resistance interfaces, increased dead space and high-resistance expiratory tubing.

What this study adds?

- This study confirms the WHO concern about CPAP quality and safety by reviewing design alterations and testing them in a lung model.
- High-resistance interfaces and narrow expiratory tubing in bCPAP systems can significantly affect CPAP delivery and imposed work of breathing, potentially introducing the risk of CPAP failure or complications.
- It is important that new designs are described correctly and compared with the original bCPAP system.

therefore often been mistaken for a bubble continuous positive airway pressure (bCPAP) system. In the original bCPAP design, as described by Sahni and Wung, the resistor clamp was replaced with wide-bore expiratory tubing submersed in water, and the interface consisted of short binasal prongs connected directly to the tubing.⁵ This design made the system pressure stable and easy to breathe through.

The simplicity of bCPAP systems makes them ideal for use in low-income and middle-income countries. In the last 10 years, new devices with several alterations from the original design have been described. Examples are provided in [table 1](#). Three design alterations of potential concern are increased interface resistance, increased system dead space and different diameters of expiratory tubing. These are summarised in [figure 1](#).



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Table 1 bCPAP design variations

	Interface resistance	Dead space	Expiratory tubing resistance	Comment
Sahni and Wung ⁵	Low	Low	Low	Used in several trials and manuscripts; Fisher & Paykel bCPAP has a similar design
Audu <i>et al</i> ⁶	High	Low	High	Description of modified oxygen cannula (figures 1–3) later used in clinical trial
Brown <i>et al</i> ³¹	Low	High	Low*	Description of the first version of the Pumani CPAP (figure 1)
Daga <i>et al</i> ⁹	High	Low	High	Clinical trial using modified oxygen cannula with seal (figures 1–5)
Duket ¹⁰	High	Low	High	Review including modified oxygen cannula (figures 2 and 3). Other designs: original bCPAP (figure 1) and high-resistance interface (RAM type, figure 5).
Kawaza <i>et al</i> ³²	Low	High	Low*	Clinical trial including Pumani first version, reference to Brown <i>et al</i>
Chisti <i>et al</i> ¹¹	High	Low	High	Randomised trial including modified oxygen cannula, reference to Duke
McAdams <i>et al</i> ²³	High	Low	Unknown	Case series and description of bCPAP with high-resistance interface (RAM type) (figure 2)
Ezenwa <i>et al</i> ¹²	High	Low	High	Retrospective observational study using modified oxygen cannula (figures 1 and 2)
WHO† ¹³	High	Low	High	Manual including modified oxygen cannula (figures 15 and 16). Other designs: original CPAP (figure 14).
Bennett <i>et al</i> ³³	High	High	Low*	Description of a bCPAP system with a high-resistance interface (RAM type) and connector tube similar to Brown <i>et al</i> (figure 1)
Falk <i>et al</i> ³⁰	Low	Low	High	Description of the second version of the Pumani CPAP (figure 2)
Bjorklund <i>et al</i> ³⁹	High	Low	High	Clinical trial using modified oxygen cannula with seal (figure 1)
Thaddanee <i>et al</i> ¹⁴	High	Unknown	High	Observational trial and description of two modified oxygen cannula systems (figures 1 and 2).
Amadi <i>et al</i> ¹⁵	High	Low	High	Observational trial and description of modified oxygen cannula systems (figure 1)

List of manuscripts with descriptions or use of bCPAP systems with design alterations from the original (top row). Dimensions are not always reported in manuscripts and some include several design variations. The figures or photographs referred to in the comment column can be found in the cited manuscripts.

*Data in the manuscript indicate that expiratory tubing resistance was not high.

†Properties refer to only one system in the manuscript. Details are provided in comment column.

bCPAP, bubble continuous positive airway pressure.

The design alterations listed previously suggest a wide variation in the design of systems referred to as bCPAP systems. The development of new systems has not been without concern: ‘Increasing use of CPAP without regulation is a concern. Many devices are in the “homemade” category; several low-cost bCPAP devices are being developed specifically for low-income countries but need to be tested for durability, reliability and safety’.⁶

Our aim was to study the effect of interface resistance and the internal diameter of the expiratory tubing on CPAP delivery and imposed work of breathing in a mechanical lung model. Large dead space in non-leakage settings is not safe and was therefore not further tested.

METHODS

Two important alterations to the original bCPAP design we identified, high-resistance interfaces and different diameters of expiratory tubing, were evaluated in a mechanical lung model.

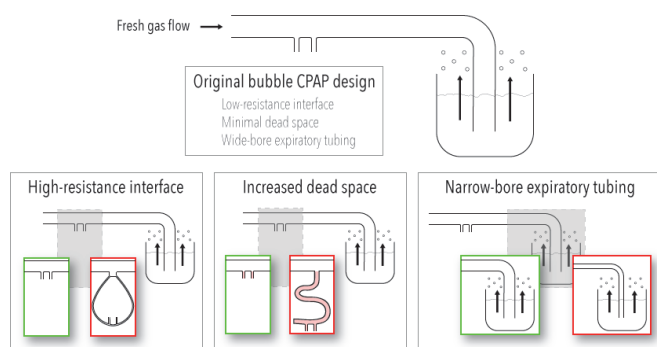


Figure 1 Summary of deviations from the original bubble CPAP system of clinical concern. Details on interface resistance, dead space and resistance of expiratory tubing presented in table 1.

Mechanical lung model

Measurements were performed using a mechanical lung model (ASL5000; Ingmar Medical, Pittsburgh, Pennsylvania, USA). Spontaneous breathing was simulated using a symmetrical, sinusoidal flow pattern with a flow maximum of 6L/min at a respiratory rate of 60 breaths/min. The main outcome was delivered CPAP and resistance to breathing. CPAP (cmH₂O) was measured as the average delivered pressure to the lung simulator. Resistance to breathing was measured as imposed work of breathing (mJ/breath).

Each interface was connected to the test lung without leakage. The driver flow was attached to the interface and the expiratory tubing was submerged in a large, open-top canister of water. The submersion depth was adjusted to 5 cm and tests were performed with non-humidified air at room temperature.

Interface resistance

To confirm the effect of interface resistance, three interfaces were tested. Two represent traditional bCPAP interfaces with short binasal prongs (Hudson prongs size 4 and Fisher & Paykel 5040 prongs). As an example of a high-resistance interface, the RAM cannula (size Infant, orange) was included.⁷ The systems made from modified nasal oxygen cannulas (table 1^{8–15}) generated too high pressures to be measured in our current setup (without leakage).

Expiratory tubing

To confirm the effects of changing the diameter of expiratory tubing, smooth tubing with a length of 1.5 m and internal diameters of 3, 4, 6, 8, 10 and 12 mm were tested. The tubing from Fisher & Paykel was included as a reference (1.47 m corrugated tubing, approximately 12 mm internal diameter).

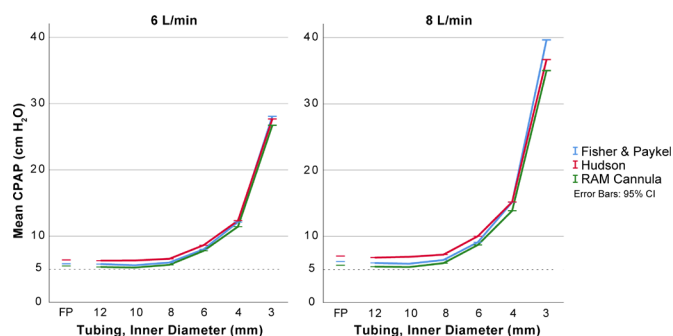


Figure 2 Effect of different interfaces and expiratory tubing diameters on mean CPAP. Mean CPAP for inner diameter expiratory tubing of 3–12 mm with three interfaces at 5 cm of submersion and with two levels of fresh gas flow. The Fisher & Paykel original expiratory tubing was included to illustrate a commercially available alternative (corrugated tubing, 1.47 m length and approximately 12 mm internal diameter). Details and statistical comparisons are available as supplementary tables. CPAP, continuous positive airway pressure.

Fresh gas flow

All systems were tested with fresh gas flows of 6 and 8 L/min calibrated with a Defender 510 (MesaLabs, California, USA) and adjusted with a standard air rotameter valve.

Analysis

Data were collected for at least 22 consecutive breaths and processed in the test lung software (Ingmar Medical) and exported to SPSS (version 25, IBM Corporation, Armonk, NY, USA). Mean values (95% CIs) were calculated for breath numbers 2–20 and compared using unpaired t-tests or analysis of variance with Games-Howell post hoc testing. Statistical significance was set to <0.05.

RESULTS

The effects on mean CPAP and imposed work of breathing by the internal diameter of expiratory tubing, the interface resistance and the fresh gas flow are displayed in figures 2 and 3 with statistical analysis in data supplements.

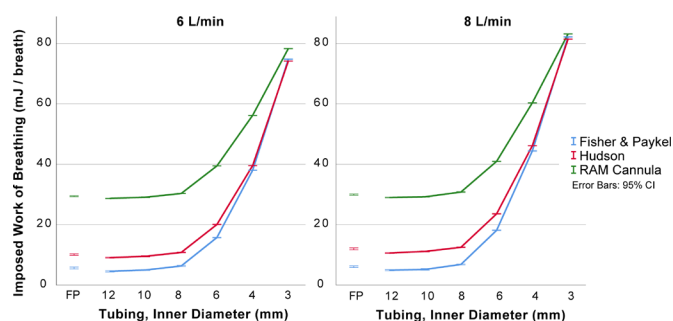


Figure 3 Effect of different interfaces and expiratory tubing diameters on mean imposed work of breathing. Resistance to breathing measured as imposed work of breathing (mJ/breath) for inner diameter expiratory tubing of 3–12 mm with three interfaces at 5 cm of submersion with two levels of fresh gas flow. The Fisher & Paykel original expiratory tubing was included to illustrate a commercially available alternative (corrugated tubing, 1.47 m length and approximately 12 mm internal diameter). Details and statistical comparisons are available as supplementary tables.

Interface resistance

There were small absolute differences in delivered CPAP pressure for the different interfaces (Hudson, RAM and Fisher & Paykel interfaces) and larger differences in imposed work of breathing between interfaces. The imposed work of breathing was highest for the RAM cannula and was most apparent with expiratory tubing with internal diameters less than 8 mm. The data are presented in figures 2 and 3, with details in online supplementary tables 1–3.

Internal diameter of expiratory tubing

With internal diameters less than 8 mm, the delivered CPAP and imposed work of breathing were increased (figures 2 and 3, with details in online supplementary tables 1–3). The increase was non-linear. With expiratory tubing at least 8 mm in internal diameter, the absolute differences in delivered CPAP were small (<1.5 cmH₂O in all comparisons).

Fresh gas flow

The delivered CPAP and imposed work of breathing increased with increasing fresh gas flows in experiments with narrow expiratory tubing. This was less pronounced for expiratory tubing with internal diameters of at least 8 mm (figures 2 and 3 with details in online supplementary tables 1–3).

DISCUSSION

After the introduction of CPAP by Gregory *et al*, several clinical studies were conducted in the 1970s and 1980s using continuous distending pressure (CDP) for newborn infants with respiratory distress syndrome (RDS).⁴ As summarised by Bancalari and Sinclair, the use of CDP reduced mortality and improved oxygenation, while early application significantly reduced the need for mechanical ventilation and the total duration of respiratory assistance.¹⁶ The use of CPAP for the treatment of RDS was common initially, but with the increased resources available for treating very-low-birthweight infants with mechanical ventilation, the CPAP technique gradually fell into disuse. However, in a few centres, bCPAP and jet CPAP treatment remained the first choice for respiratory support for infants in respiratory distress.^{17–20} In recent times, a paradigm shift has occurred, and CPAP is now the evidence-based choice for initial treatment of infants with respiratory distress.

We refer to the original design and basic principles of bCPAP as a system with short binasal prongs, no dead space and wide-bore expiratory tubing. The origin of this system has not been published, but it has been used at Columbia University, New York, since the mid-1970s (JT Wung and R Sahni, personal communication 2019). These principles have also been applied in commercial systems for neonates such as the Fisher & Paykel bCPAP system.

To meet the need for CPAP systems that can be used in low-resource settings, novel systems have been developed and are in clinical use. Although presented as bCPAP, many of these systems deviate from the basic principles of the original bCPAP design as presented in figure 1 and table 1. Our mechanical test lung simulations confirm that these alterations can have negative effects on performance.

Interfaces

Short binasal prongs or nasal masks are the recommended interface when providing CPAP to infants.^{21 22} Several other interfaces are widely used for CPAP treatment. The RAM cannula interface has been used for providing CPAP and nasal intermittent

positive pressure ventilation.^{23–26} This is not Food and Drug Administration approved, and the use is off-label. In our tests, the RAM cannula interface had a higher resistance to breathing than short binasal prongs. This is consistent with prior studies.⁷ Our results indicate that using a high-resistance interface like the RAM cannula, with a seal at the nares and closed mouth, might lead to an unintentionally high resistance to breathing.

Devices made from a modified standard oxygen cannula will have high resistance due to the narrow diameters. These were used in some trials included in [table 1](#) but not included in our study as they generated pressures well above our equipment range when tested without leakage.

These designs combine a high-resistance interface with high-resistance tubing and have characteristics that are probably closer to high-flow nasal cannula (HFNC) systems than the original bCPAP.

Expiratory tubing

The resistance of expiratory tubing adds pressure to the CPAP generated by the submersion depth. The resulting CPAP will be higher than intended, and this is not reflected by the submersion depth ([figure 2](#)). Our findings confirm results from previous studies. Mestriner *et al* investigated this in positive-expiratory-pressure (PEP) therapy bottles for adults,²⁷ and Wu *et al* recorded an increase in CPAP with increased expiratory limb resistance.²⁸ The increased tubing resistance also leads to increased resistance to breathing ([figure 3](#)). This is expected and has been shown for other systems that generate CPAP using outflow resistance.^{29 30}

With a 1.5 m expiratory tube, together with a fresh gas flow of 8 L/min or less, the diameter needs to be at least 8 mm to avoid a higher CPAP level than intended.

Dead space

Although known for decades, the issue of dead space and risk of rebreathing is sometimes neglected when modifying the original bCPAP design.^{31–33} Without leakage, the use of long connecting tubing to an interface can lead to rebreathing and respiratory failure due to large dead space. At least two systems were identified that had neglected the issue of large dead space in their design.^{31–33}

The risk of rebreathing with large dead space should always be considered when designing new bCPAP systems and should be avoided.

Flow

The driver flow for the original bCPAP design can be adjusted to compensate for leakage and peak inspiratory flows.³⁴ For systems with high-resistance expiratory tubing, the increase in pressure above submersion depth will be more pronounced with higher driver flows ([figure 2](#)). For these systems and those using a high-resistance interface, recommendations on driver flows are difficult to give. Some systems have been observed to bubble even if no patient is connected.^{35 36}

High-flow nasal cannula

HFNC has gained popularity as respiratory support in recent years because of its light weight and simplicity. The European RDS guidelines suggest that HFNC can be used during weaning as an alternative to CPAP.²¹ Both the HIPSTER trial and the HUNTER trial showed higher failure rates for HFNC compared with CPAP when used as primary respiratory support in preterm infants.^{37 38}

CPAP systems in [table 1](#) and designs in [figure 1](#) with high-resistance expiratory tubing and a high-resistance interface, such as the modified oxygen cannula systems, resemble HFNC systems more than the original bCPAP systems. With a very high delivered pressure, unrelated to submersion depth, and a high-resistance interface, it is not likely that the infant can breathe through the device. Instead, the infant will be depending on leakage to avoid high resistance to breathing and excessive CPAP. These hybrid systems are not traditional CPAP systems nor dedicated HFNC systems. When used with a seal, they are potentially dangerous, equivalent to using an HFNC without assuring leakage.

We are not aware of any trials comparing these hybrid systems to the original bCPAP system. A trial by Chisti *et al* compared a modified oxygen cannula system, labelled as bCPAP, to low-flow and high-flow oxygen.¹¹ The trial was stopped early because of higher clinical failure in the low-flow oxygen treatment group. It did not include an original bCPAP system. There is no evidence that the hybrid systems have a treatment effect equivalent to original bCPAP systems or commercial HFNC systems.

We recommend that bCPAP systems that apply the principles of the original design should be available as primary or rescue therapy for infants with more severe respiratory distress as they have a greater need for distending pressure to aid lung expansion. This could lead to less treatment failure and increased survival.

Limitations

The mechanical lung tests were designed to confirm and illustrate the effect of alterations from the basic principles of bCPAP. This means that not all systems, CPAP levels, tubing alternatives or flows were included. This article focused on design variations, and the risks of nasal trauma, humidification, gas supply, oscillations and costs were not discussed. The tests were performed without leakage. The very high CPAP pressures seen with narrow-bore expiratory tubing will result in leakage at the nose, through the mouth or to the gut.

SUMMARY

Our study shows significant effect on CPAP delivery and imposed work of breathing with changes in resistance of nasal interface and expiratory tubing. Narrow expiratory tubing resulted in higher CPAP levels than indicated by the submersion depth. Several of the systems referred to as bCPAP deviate from the original bCPAP principles, and some of the reviewed designs are better described as HFNC hybrids. New systems should be described correctly and compared with the original bCPAP.

The next logical step is to recognise these differences and to develop a strategy where the original bCPAP is used as primary treatment when available or as backup if simpler systems are failing. New systems should be introduced with caution and functionally defined as high-flow, hybrid or original bCPAP systems. Referring to all systems that bubble as bCPAP is misleading and potentially hazardous. Trials confirming the effectiveness and safety of new systems should be encouraged, and the original system should be used as the gold standard in such trials.

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Contributors All authors (SB, MF, SD, BJ and TD) had full access and were active in writing and reviewing the manuscript. Data collection and analysis were mainly performed by MF.

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Competing interests None declared.

Patient consent for publication Not required.

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Provenance and peer review Not commissioned; externally peer reviewed.

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Flow	ID (mm)	Fisher & Paykel				Hudson				RAM			
		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)	
		Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)
6 L/min	3	28.1 (28,06-28,12)		74.8 (74,66-74,89)		27.7 (27,66-27,71)		74.2 (74,09-74,23)		26.7 (26,70-26,77)		78.3 (78,19-78,40)	
	4	12.1 (12,10-12,14)		38.0 (37,90-38,09)		12.3 (12,33-12,35)		39.6 (39,49-39,61)		11.4 (11,43-11,45)		56.2 (56,09-56,26)	
	6	8.0 (8,00-8,03)		15.8 (15,63-15,87)		8.6 (8,62-8,65)		20.1 (19,94-20,18)		7.8 (7,76-7,79)		39.5 (39,38-39,52)	
	8	6.0 (5,99-6,03)		6.3 (6,17-6,49)		6.6 (6,55-6,60)		10.8 (10,69-10,91)		5.7 (5,65-5,67)		30.3 (30,23-30,41)	
	10	5.6 (5,59-5,62)		5.0 (4,85-5,12)		6.3 (6,30-6,34)	a	9.5 (9,32-9,76)		5.3 (5,24-5,27)		29.1 (28,93-29,22)	
	12	5.8 (5,76-5,80)		4.6 (4,37-4,77)		6.3 (6,28-6,32)	a	9.1 (8,91-9,21)		5.3 (5,32-5,36)		28.7 (28,57-28,80)	
	FP	5.8 (5,80-5,85)		5.7 (5,35-5,99)		6.4 (6,37-6,43)		10.1 (9,84-10,35)		5.5 (5,48-5,51)		29.4 (29,29-29,58)	
8 L/min	3	39.7 (39,61-39,72)		82.2 (82,04-82,27)		36.7 (36,66-36,74)		81.4 (81,33-81,49)		35.0 (34,98-35,08)		83.1 (83,02-83,22)	
	4	15.2 (15,14-15,18)		44.4 (44,28-44,52)		15.2 (15,19-15,21)		46.1 (46,06-46,20)		13.9 (13,85-13,89)		60.3 (60,22-60,42)	
	6	9.1 (9,10-9,14)		18.1 (18,01-18,25)		10.0 (10,01-10,03)		23.6 (23,50-23,68)		8.7 (8,69-8,71)		41.0 (40,85-41,07)	
	8	6.4 (6,42-6,45)		6.8 (6,70-6,96)		7.2 (7,23-7,26)		12.5 (12,39-12,61)		6.0 (5,94-5,97)		30.8 (30,67-30,92)	
	10	5.9 (5,85-5,89)		5.2 (4,93-5,45)	A	6.9 (6,88-6,93)		11.2 (10,97-11,32)		5.4 (5,35-5,38)		29.2 (29,08-29,36)	B
	12	6.0 (5,96-5,99)		4.9 (4,73-5,11)	A	6.8 (6,77-6,82)		10.6 (10,49-10,74)		5.4 (5,41-5,44)		29.0 (28,87-29,10)	B
	FP	6.2 (6,17-6,22)		6.1 (5,84-6,37)		7.0 (7,02-7,06)		12.0 (11,67-12,29)		5.6 (5,61-5,65)		30.0 (29,76-30,15)	

Supplementary Table 1: Effect of different internal diameter of expiratory tubing.

Means and confidence intervals are given for both pressure (white background) and imposed work of breathing (gray background). Multiple comparisons of means were made for 19 consecutive breaths with a Games-Howell correction and $p < 0.05$ was considered significant. Non-significant comparisons are indicated columnwise by letters (a, A-B). The original Fisher & Paykel tubing (FP) was included for reference.

Flow	ID (mm)	Fisher & Paykel				Hudson				RAM			
		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)	
		Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)
6 L/min	3	28.1 (28,06-28,12)		74.8 (74,66-74,89)		27.7 (27,66-27,71)		74.2 (74,09-74,23)		26.7 (26,70-26,77)		78.3 (78,19-78,40)	
	4	12.1 (12,10-12,14)		38.0 (37,90-38,09)		12.3 (12,33-12,35)		39.6 (39,49-39,61)		11.4 (11,43-11,45)		56.2 (56,09-56,26)	
	6	8.0 (8,00-8,03)		15.8 (15,63-15,87)		8.6 (8,62-8,65)		20.1 (19,94-20,18)		7.8 (7,76-7,79)		39.5 (39,38-39,52)	
	8	6.0 (5,99-6,03)		6.3 (6,17-6,49)		6.6 (6,55-6,60)		10.8 (10,69-10,91)		5.7 (5,65-5,67)		30.3 (30,23-30,41)	
	10	5.6 (5,59-5,62)		5.0 (4,85-5,12)		6.3 (6,30-6,34)		9.5 (9,32-9,76)		5.3 (5,24-5,27)		29.1 (28,93-29,22)	
	12	5.8 (5,76-5,80)		4.6 (4,37-4,77)		6.3 (6,28-6,32)		9.1 (8,91-9,21)		5.3 (5,32-5,36)		28.7 (28,57-28,80)	
	FP	5.8 (5,80-5,85)		5.7 (5,35-5,99)		6.4 (6,37-6,43)		10.1 (9,84-10,35)		5.5 (5,48-5,51)		29.4 (29,29-29,58)	
8 L/min	3	39.7 (39,61-39,72)		82.2 (82,04-82,27)		36.7 (36,66-36,74)		81.4 (81,33-81,49)		35.0 (34,98-35,08)		83.1 (83,02-83,22)	
	4	15.2 (15,14-15,18)		44.4 (44,28-44,52)		15.2 (15,19-15,21)		46.1 (46,06-46,20)		13.9 (13,85-13,89)		60.3 (60,22-60,42)	
	6	9.1 (9,10-9,14)		18.1 (18,01-18,25)		10.0 (10,01-10,03)		23.6 (23,50-23,68)		8.7 (8,69-8,71)		41.0 (40,85-41,07)	
	8	6.4 (6,42-6,45)		6.8 (6,70-6,96)		7.2 (7,23-7,26)		12.5 (12,39-12,61)		6.0 (5,94-5,97)		30.8 (30,67-30,92)	
	10	5.9 (5,85-5,89)		5.2 (4,93-5,45)		6.9 (6,88-6,93)		11.2 (10,97-11,32)		5.4 (5,35-5,38)		29.2 (29,08-29,36)	
	12	6.0 (5,96-5,99)		4.9 (4,73-5,11)		6.8 (6,77-6,82)		10.6 (10,49-10,74)		5.4 (5,41-5,44)		29.0 (28,87-29,10)	
	FP	6.2 (6,17-6,22)		6.1 (5,84-6,37)		7.0 (7,02-7,06)		12.0 (11,67-12,29)		5.6 (5,61-5,65)		30.0 (29,76-30,15)	

Supplementary Table 2: Effect of different interfaces.

Means and confidence intervals are given for both mean pressure (white background) and imposed work of breathing (gray background). Multiple comparisons of means were made for 19 consecutive breaths for different interfaces with a Games-Howell correction and $p < 0.05$ was considered significant. All comparisons were significant. The original Fisher & Paykel tubing (FP) was included for reference.

System		6 L/min				8 L/min			
		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)		Pressure (cm H ₂ O)		Imposed Work of breathing (mJ/breath)	
ID (mm)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	Mean	CI (95%)	
Fisher & Paykel	3	28.1 (28,06-28,12)	74.8 (74,66-74,89)	39.7 (39,61-39,72)	82.2 (82,04-82,27)				
	4	12.1 (12,10-12,14)	38.0 (37,90-38,09)	15.2 (15,14-15,18)	44.4 (44,28-44,52)				
	6	8.0 (8,00-8,03)	15.8 (15,63-15,87)	9.1 (9,10-9,14)	18.1 (18,01-18,25)				
	8	6.0 (5,99-6,03)	6.3 (6,17-6,49)	6.4 (6,42-6,45)	6.8 (6,70-6,96)				
	10	5.6 (5,59-5,62)	5.0 (4,85-5,12)	5.9 (5,85-5,89)	5.2 (4,93-5,45)				
	12	5.8 (5,76-5,80)	4.6 (4,37-4,77)	6.0 (5,96-5,99)	4.9 (4,73-5,11)				
	FP	5.8 (5,80-5,85)	5.7 (5,35-5,99)	6.2 (6,17-6,22)	6.1 (5,84-6,37)				
Hudson	3	27.7 (27,66-27,71)	74.2 (74,09-74,23)	36.7 (36,66-36,74)	81.4 (81,33-81,49)				
	4	12.3 (12,33-12,35)	39.6 (39,49-39,61)	15.2 (15,19-15,21)	46.1 (46,06-46,20)				
	6	8.6 (8,62-8,65)	20.1 (19,94-20,18)	10.0 (10,01-10,03)	23.6 (23,50-23,68)				
	8	6.6 (6,55-6,60)	10.8 (10,69-10,91)	7.2 (7,23-7,26)	12.5 (12,39-12,61)				
	10	6.3 (6,30-6,34)	9.5 (9,32-9,76)	6.9 (6,88-6,93)	11.2 (10,97-11,32)				
	12	6.3 (6,28-6,32)	9.1 (8,91-9,21)	6.8 (6,77-6,82)	10.6 (10,49-10,74)				
	FP	6.4 (6,37-6,43)	10.1 (9,84-10,35)	7.0 (7,02-7,06)	12.0 (11,67-12,29)				
RAM	3	26.7 (26,70-26,77)	78.3 (78,19-78,40)	35.0 (34,98-35,08)	83.1 (83,02-83,22)				
	4	11.4 (11,43-11,45)	56.2 (56,09-56,26)	13.9 (13,85-13,89)	60.3 (60,22-60,42)				
	6	7.8 (7,76-7,79)	39.5 (39,38-39,52)	8.7 (8,69-8,71)	41.0 (40,85-41,07)				
	8	5.7 (5,65-5,67)	30.3 (30,23-30,41)	6.0 (5,94-5,97)	30.8 (30,67-30,92)				
	10	5.3 (5,24-5,27)	29.1 (28,93-29,22)	5.4 (5,35-5,38)	29.2 (29,08-29,36)				
	12	5.3 (5,32-5,36)	28.7 (28,57-28,80)	5.4 (5,41-5,44)	29.0 (28,87-29,10)				
	FP	5.5 (5,48-5,51)	29.4 (29,29-29,58)	5.6 (5,61-5,65)	30.0 (29,76-30,15)				

Supplementary Table 3: Effect of two different driver flows.

Means and confidence intervals given for pressure (white background) and imposed work of breathing (gray background). Un-paired t-tests were performed comparing the two different flows and $p < 0.05$ was considered significant. The non-significant comparison is indicated rowwise by letter (A). The original Fisher & Paykel tubing (FP) was included for reference.